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## **Voltage Flicker Estimation Based on Pair of Inter-harmonics Analysis Method**

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#### ABSTRACT

This paper presents a voltage flicker estimation based on a pair of inter-harmonics analysis method. The proposed algorithm is able to estimate flicker frequency and amplitude changes of a voltage waveform. The correlation of the pair of inter-harmonics, flicker frequency, and amplitude changes are presented and their formulas highlighted. Experimental results indicate the amplitude of pair of inter-harmonics can detect the voltage flicker. Furthermore, the experimental results are compared with the measurement results obtained by using the Fluke power analyzer (Pst).

Keywords: voltage flicker, inter-harmonics, FFT

#### **INTRODUCTION**

Nowadays, utilization of nonlinear loads with asymmetrical current-voltage characteristics such as arc motor drive and arc furnace creates voltage fluctuation to the power system (Grady & Santoso, 2001). Specifically, voltage fluctuation with certain frequency value is considered as voltage flicker (Tayjasanant, Wencong, Chun, & Wilsun, 2005). Moreover,

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Some of research works have been conducted to improve the accuracy of the IEC flickermeter (Virulkar & Aware, 2012) and voltage flicker mitigation have also been done by many researchers (Michel & de Preville, 2004; Routimo et al., 2008). Analysis on reducing the observation time of Pst (Tan & Ramachandaramurthy, 2012) has also been done by researchers. Interrelationship between inter-harmonics and voltage flicker has been investigated by many researchers too (Dahai, Wilsun, & Nassif, 2005; Keppler, Watson, Arrillaga, & Shiun, 2003; Langella, Liccardo, Marino, Testa, & Triggianese, 2007; Tayjasanant et al., 2005; Wilsun, 2005). Voltage flicker detection has been proposed by many researchers such as atomic method (Ning, Linchuan, & Qingquan, 2012), wavelet Fourier transform (WeiHui & ShiPing, 2011), Chirp-z transform (Kang, Guo, Li, & Yan, 2010), and new modified S-transform algorithm (Huang, Xu, Shi, & Zhang, 2014). The atomic method is considered not practical since it needs a special voltage flicker dictionary which is generated by matching pursuits algorithm. The voltage flicker detection based on wavelet Fourier transform is mathematically considered cumbersome as the measured waveform needs to be filtered by wavelet transform, and then use a long window is required to identify the voltage flicker amplitude and flicker frequency. Other than that, the Chirp-z transform is only tested in simulation and it is not practical as the algorithm is not tested with noise condition. Then, the modified S-transform for voltage flicker detection algorithm is able to detect duration time of voltage flicker effectively but it cannot detect severity of voltage flicker.

Basically, there are some changes on the amplitudes of pair of inter-harmonics due to intrinsic characteristic of a voltage flicker waveform (Jing, Tayjasanant, Wilsun, & Caixin, 2008). This proposed algorithm is able to estimate flicker frequency and amplitude changes in a voltage waveform based on pair of inter-harmonics analysis method. Firstly, amplitudes of pair of inter-harmonics are detected by signal processing method. Then, the amplitudes of particular inter-harmonics are substituted in the formulas that have been generated in this paper. Subsequently, the flicker frequency and amplitude changes of a voltage flicker waveform are detected and are compare with the flicker reference curve in order to detect the voltage flicker.

A number of signal processing algorithms based on different techniques for inter-harmonics detection such as Discrete Fourier Transform (DFT), Fast Fourier Transform (FFT), Short-Time Fourier transform (STFT) (Wright, 1999) and spectrogram (Abdullah, Peng, Ghani, & Jopri, 2014) have been reported over the past years (Coppola, Qian, Buso, Boroyevich, & Bell, 2008). The FFT is considered direct improvement of the DFT which is able to perform faster conversion from time to frequency domain, but number of samples must fulfil 2n where n is an integer number. Otherwise, operation of the FFT may lead to inaccurate result due to phenomena of aliasing (Hsiung-Cheng, 2008), leakage (Chang, Chen, Liu, & Wu, 2008), and picket fence effects (Chang et al., 2008). Meanwhile, STFT is considered improvement of the FFT as it is generated based on sliding FFT process. The sliding FFT is done by dividing the measurement signal into many small divisions and FFT is applied to these tiny divisions. Next, spectrogram is considered as squared magnitude of the STFT and the output of spectrogram are plotted in spectrograph. Subsequently, the STFT and spectrogram are considered mathematical burden due to many times of applying FFT. Therefore, directly using FFT is merited, to be utilized in the proposed algorithm due to its speed capability to convert time domain to frequency domain. The correlation between voltage flicker and inter-harmonics are presented in Section II. Sections III discusses the background of the FFT. Section IV presents the proposed algorithm. The experiments are presented in Sections VI. Lastly, the conclusion is contained in Section VI.

## CORRELATION BETWEEN INTER-HARMONICS AND VOLTAGE FLICKER

Basically, modulated waveform can occur following the appearance of inter-harmonics in a power system. The fluctuation frequency of the instantaneous voltage is considered as voltage flicker frequency. The voltage flicker frequency (Jing et al., 2008), fflicker can be calculated by

$$f_{flicker} = \left| f_{IH} - f_f \right| \tag{1}$$

where,  $f_{IH}$  and  $f_f$  are considered as inter-harmonic frequency and fundamental frequency respectively of the power system. By considering a 50 Hz power system which consists of 3 Hz of voltage flicker frequency, then the related inter-harmonics are 47 Hz and 53 Hz. Essentially, the voltage flicker may occur due to pair of inter-harmonics (47 and 53 Hz together) or single inter-harmonic (47 or 53 Hz). In practical situation, voltage flicker waveform occurs mainly due to pair of inter-harmonics. Therefore, the derivation of formula for aforementioned situation is shown as follow (Zai Peng, Radzi, Hizam, & Abdul Wahab, 2015):

$$v_2(t) = \alpha_3 e^{j\omega_3 t} + \alpha_1 e^{j\omega_1 t} + \alpha_2 e^{j\omega_2 t}$$
(2)

 $v_2(t)$ ,  $\alpha_1$ , and  $\omega_1$  are represented as the instantaneous voltage, fundamental amplitude, and angular frequency (fundamental) respectively. Meanwhile,  $\alpha_2$ , and  $\omega_2$  are symbolized as the first inter-harmonic amplitude, and its angular frequency. Next,  $\alpha_3$ , and  $\omega_3$  are represented as the second inter-harmonic amplitude, and its angular frequency respectively. The relationship of  $\omega$  is assumed as  $\omega_3 < \omega_1 < \omega_2$ .

After that, the aforementioned instantaneous voltage becomes,

$$v_{2}(t) = e^{j\omega_{1}t} \left(\alpha_{1} + \alpha_{2} e^{j(\omega_{2} - \omega_{1})t} + \alpha_{3} e^{j(\omega_{3} - \omega_{1})t}\right)$$
(3)

 $e^{j\omega_1}t$  is represented as factorized exponential form of fundamental frequency. The amplitude is represented as  $\alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_2)t} + \alpha_3 e^{j(\omega_3 - \omega_2)t}$ . Therefore, the amplitude can be calculated as following:

$$Amp_{2H} = \left| \alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_1)t} + \alpha_3 e^{j(\omega_3 - \omega_1)t} \right| \tag{4}$$

After the expansion,

$$Amp_{\cdot 2H} = \begin{vmatrix} \alpha_1 + \alpha_2 \cos(\omega_2 - \omega_1)t + j\alpha_2 \sin(\omega_2 - \omega_1)t \\ + \alpha_3 \cos(\omega_3 - \omega_1)t + j\alpha_3 \sin(\omega_3 - \omega_1)t \end{vmatrix}$$
(5)

The calculation for the amplitude is as follow:

$$Amp_{2H} = \sqrt{\left[\frac{\alpha_1 + \alpha_2 \cos(\omega_2 - \omega_1)t}{\alpha_3 \cos(\omega_3 - \omega_1)t}\right]^2 + \left[\alpha_2 \sin(\omega_2 - \omega_1)t + \alpha_3 \sin(\omega_3 - \omega_1)t\right]^2}$$
(6)

Further elaboration is:

$$Amp_{\cdot_{2H}} = \sqrt{\begin{bmatrix} 2\alpha_{1}\alpha_{2}\cos(\omega_{2}-\omega_{1})t + 2\alpha_{1}\alpha_{3}\cos(\omega_{3}-\omega_{1})t + 2\alpha_{2}\alpha_{3}\cos(\omega_{2}-\omega_{1})t\cos(\omega_{3}-\omega_{1})t + \alpha_{2}^{2}\cos^{2}(\omega_{2}-\omega_{1})t + \alpha_{3}^{2}\cos^{2}(\omega_{3}-\omega_{1})t + \alpha_{2}^{2}\sin^{2}(\omega_{2}-\omega_{1})t + \alpha_{3}^{2}\sin^{2}(\omega_{3}-\omega_{1})t + \alpha_{3}^{2}\cos^{2}(\omega_{3}-\omega_{1})t + \alpha$$

Since

$$\omega_3 p \,\omega_1 p \,\omega_2 and \,\omega_3 - \omega_1 = \omega_2 - \omega_1 \tag{8}$$

Then,

$$Amp_{\cdot_{2H}} = \sqrt{\begin{bmatrix} 2\alpha_{1}\alpha_{2}\cos(\omega_{2}-\omega_{1})t + 2\alpha_{1}\alpha_{3}\cos(\omega_{3}-\omega_{1})t + 2\alpha_{2}\alpha_{3}\cos^{2}(\omega_{2}-\omega_{1})t + \alpha_{1}^{2} + \\ \alpha_{2}^{2}\cos^{2}(\omega_{2}-\omega_{1})t + \alpha_{3}^{2}\cos^{2}(\omega_{3}-\omega_{1})t + \alpha_{2}^{2}\sin^{2}(\omega_{2}-\omega_{1})t + \\ 2\alpha_{2}\alpha_{3}\sin^{2}(\omega_{2}-\omega_{1})t + \alpha_{3}^{2}\sin^{2}(\omega_{3}-\omega_{1})t \end{bmatrix}}$$
(9)

By simplifying using trigonometry identity:

$$4mp_{\cdot_{2H}} = \sqrt{\left[2\alpha_{1}\alpha_{2}\cos(\omega_{2}-\omega_{1})t + 2\alpha_{1}\alpha_{3}\cos(\omega_{3}-\omega_{1})t + 2\alpha_{2}\alpha_{3} + \alpha_{1}^{2} + \alpha_{2}^{2} + \alpha_{3}^{2}\right]}$$
(10)

Therefore, the simplified version is:

$$Amp_{2H} = \sqrt{\left[2\alpha_{1}(\alpha_{2} + \alpha_{3})\cos(\omega_{2} - \omega_{1})t + 2\alpha_{2}\alpha_{3} + \alpha_{1}^{2} + \alpha_{2}^{2} + \alpha_{3}^{2}\right]}$$
(11)

The maximum of the instantaneous voltage is:

$$Amp_{2H}max = \sqrt{\left[2\alpha_{1}(\alpha_{2} + \alpha_{3})(1) + 2\alpha_{2}\alpha_{3} + \alpha_{1}^{2} + \alpha_{2}^{2} + \alpha_{3}^{2}\right]}$$
(12)

The minimum of the instantaneous voltage is:

$$Amp_{2H}\min = \sqrt{\left[2\alpha_{1}(\alpha_{2} + \alpha_{3})(-1) + 2\alpha_{2}\alpha_{3} + \alpha_{1}^{2} + \alpha_{2}^{2} + \alpha_{3}^{2}\right]}$$
(13)

The substitution of the  $\cos(\omega_2 - \omega_1)$ t to 1 and -1 is for calculating the maximum and minimum values of the instantaneous voltage respectively. Figure 1 shows voltage flicker waveform for 50 Hz voltage supply with presence of pair of inter-harmonics, in which 47 Hz ( $\omega_3$ ) and 53 Hz ( $\omega_2$ ) with amplitude of 0.1 p.u. ( $\alpha_3$ ) and 0.2 p.u. ( $\alpha_2$ ) respectively. The maximum and minimum values of the instantaneous voltage in Figure 1(b) are 1.3 and 0.7 p.u respectively. Assuming the amplitudes of  $\alpha_3$ ,  $\alpha_1$  and  $\alpha_2$  are determined to be 0.1, 1 and 0.2 p.u. respectively Eq. (12) and

#### Inter-harmonics Analysis for Voltage Flicker Estimation



*Figure 1*. Voltage flicker waveform caused by pair of inter-harmonics: (a) zoom-out version, and (b) zoom-in version

eq. (13) is used to calculate the maximum and minimum values of the instantaneous voltage, which are 1.3 and 0.7 p.u. respectively. To evaluate severity of the voltage flicker, relative fluctuation voltage ( $\Delta v/v$ ) has to be calculated based on the following formula:

$$\Delta v / v = \frac{Amp_{2H} \cdot \max - Amp_{2H} \cdot \min}{\alpha_1} \times 100$$
(14)

For Figure 1,  $\Delta v/v$  is 60%. Again, the amplitudes of fundamental ( $\alpha$ 1) and two inter-harmonics ( $\alpha_2$  and  $\alpha_3$ ) are the key values to identify  $\Delta v/v$ .

To summarize, a generated voltage flicker may produce significant effect on the amplitudes of a pair of inter-harmonics (Jing et al., 2008). The amplitudes of fundamental ( $\alpha_1$ ) and pair of inter-harmonics ( $\alpha_2$  and  $\alpha_3$ ) is found to be crucial in order to identify  $\Delta v/v$  and is discussed in the next section.

#### **BACKGROUND OF FFT**

Based on standard IEC 61000-4-7, the general formula for FFT is

$$X(k) = \sum_{n=1}^{N-1} x(n) e^{-j\omega_{k}n}$$
(15)

where,

$$\omega_k = \frac{2\pi k}{N} \tag{16}$$

N is number of samples in time domain; k is number of samples in frequency domain (Bin number returned by FFT); x is data in time domain and X is data in frequency domain. Since

$$e^{-j\omega_{k}n} = \cos\left(\frac{2\pi kn}{N}\right) - j\sin(\frac{2\pi kn}{N})$$
(17)

Then, the output of the FFT in frequency domain is

$$X(k) = \sum_{n=1}^{N-1} \left[ x(n) \cos\left(\frac{2\pi kn}{N}\right) - jx(n) \sin\left(\frac{2\pi kn}{N}\right) \right]$$
(18)

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It can be written as

$$X(k) = \sum_{j=1}^{N-1} [real - j\_imaginary]$$
<sup>(19)</sup>

After that, the amplitude and phase values of the desired signal can be extracted via following equation:

$$A = \sqrt{real^2 + imaginary^2} \tag{20}$$

$$\theta = \tan^{-1} \frac{imaginary}{real} \tag{21}$$

Based on previous works, optimized sampling frequency for FFT is 12.8k Hz (Leelajindakrairerk & Chompoo-Inwai, 2012; Yamada, 2013) for detecting signal with fundamental frequency of 50 Hz. Specifically, the frequency resolution (eq. (22)) is needed for this proposed algorithm is 0.1. Therefore, the window size is 128k samples (12.8k/0.1). Consequently, 10s is needed for processing a single output data.

$$Frequency\_resolution = \frac{Sampling\_frequency}{Window\_size}$$
(22)

#### **PROPOSED ALGORITHM**

As discussed earlier, the amplitudes of pair of inter-harmonics and fundamental frequency are the key values to determine the voltage flicker. Principally, FFT is utilized as the amplitudes detector due to its advantages as mentioned in the introduction section. The particular amplitudes' values are substituted into eq. (12) and eq. (13) to determine the maximum and minimum values of the fluctuation voltage and the relative fluctuation voltage ( $\Delta v/v$ ) calculated via eq. (14). The voltage flicker can be detected by comparing  $\Delta v/v$  with voltage flicker reference curve. Specifically, voltage flicker is detected when then  $\Delta v/v$  is positioned above the flicker reference curve (Figure 3) and vice versa. The voltage flicker reference curve is generated based on IEC standard (Albistur, Aravena, Moran, & Espinoza, 2014). The block diagram of the proposed algorithm is shown in Figure 2.



*Figure 2*. VBlock diagram of the proposed algorithm

Figure 3. Voltage flicker reference curve

#### **EXPERIMENTAL RESULTS**

Figure 4 shows the experimental setup to perform this proposed algorithm. Programmable AC source model 6590 is utilized as voltage flicker waveform generator for this experimental setup. Furthermore, several voltage flicker waveforms are considered in this experimental work for further evaluating robustness of the proposed algorithm. The benchmarking tool used is Fluke power analyzer (P<sup>st</sup>). Data acquisition is assessed using differential probe Gw Instek GDP\_025 and Ni USB 6212. Sampling frequency of 12,800 Hz is utilized for this experimental work. The window width is 128k samples. Therefore, 10 seconds are needed for single experimental data. Finally, the data is exported to Matlab Simulink to further be analysed by the proposed algorithm as shown in Figure 2.



*Figure 4.* Configuration block for the experimental work

Figure 5. Data analysis for the experimental work

The programmable AC source is supplied by a voltage (rms) of 240 V and the aforementioned voltage waveform is interrupted by various envelope pulse levels which are generated by the programmable AC source too. Two types of envelope pulses level voltage (rms) are utilized in this experimental setup, which are 239.5 and 237 V. In addition, single envelope pulse level is programmed with various pulse frequencies such as 0.1, 0.5, 1, 5 and 10 Hz. Subsequently, 10 sets of experimental data are used for testing. Table 1 is a summary of the data analysis related to this experimental work. FFT is utilized to capture and analyse the voltage flicker waveform generated by the programmable AC source and the maximum, minimum and relative fluctuation voltages are generated by substituting the outputs of the FFT to eq. (12), eq. (13) and eq. (14) accordingly. The voltage flicker is detected, when the value of relative fluctuation voltage (eq. (14)) is located above the flicker reference curve (Figure 5). The Fluke power analyzer (P<sub>st</sub>) is utilized for benchmarking purposes where the voltage flicker is detected when the P<sub>st</sub> is greater than 1. The voltage flicker is successfully detected via the proposed algorithm, which is compared with the Fluke power analyzer (P<sub>st</sub>) to ensure 100% detection accuracy.

Pulse level (Vrms)	Pulse frequency/ Flicker frequency (Hz)	Number of test	FFT			Calculation by proposed algorithm				FLUKE		Detection
			50 Hz- Pulse frequency	50 Hz	50 Hz+ Pulse frequency	Max (Vpeak)	Min (Vpeak)	%∆v/v	Flicker detection	(P <sub>st</sub> )	Flicker detection (Pst>1)	Accuracy (%)
239.50	0.10	1	1.03	336.90	0.77	338.70	335.10	1.07	No	0.16	No	100
237.00		2	1.65	335.10	1.56	338.31	331.89	1.92	Yes	1.05	Yes	100
239.50	0.50	3	0.27	336.90	0.26	337.43	336.37	0.32	No	0.23	No	100
237.00		4	1.42	335.10	1.28	337.80	332.40	1.61	Yes	1.53	Yes	100
239.50	1.00	5	0.14	336.90	0.28	337.31	336.49	0.25	No	0.26	No	100
237.00		6	1.33	335.10	1.37	337.80	332.40	1.61	Yes	1.78	Yes	100
239.50	5.00	7	0.19	336.90	0.21	337.30	336.50	0.24	No	0.45	No	100
237.00		8	1.30	335.10	1.38	337.78	332.42	1.60	Yes	3.02	Yes	100
239.50	10.00	9	0.22	336.90	0.19	337.31	336.49	0.24	No	0.65	No	100
237.00		10	1.35	335.10	1.34	337.79	332.41	1.60	Yes	4.36	Yes	100

 Table 1

 Summary of data analysis for the proposed algorithm (Experimental

## CONCLUSION

This paper has presented voltage flicker detection based on pair of inter-harmonics analysis method. The amplitudes of pair of inter-harmonics and fundamental frequency are shown to be the key values for determining the voltage flicker. The amplitude of the aforementioned inter-harmonics was substituted into the formula that have been derived in this paper accordingly. Subsequently, The voltage flicker can be detected when the relative fluctuation voltage is located above with the flicker reference curve. According to experimental results, the amplitudes of pair of inter-harmonics are able to detect the voltage flicker. The experimental results were compared with those obtained by using the Fluke power analyzer ( $P_{st}$ ).

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